

SPECIFICATION

RESIN COMPOUND FOR FABRICATING INTERLAYER DIELECTRIC OF  
PRINTED WIRING BOARD, RESIN SHEET AND RESIN APPLIED-COPPER  
5 FOIL FOR FORMING INSULATING LAYER USING THE RESIN COMPOUND,  
AND COPPER-CLAD LAMINATE USING THEM

TECHNICAL FIELD

The present invention relates to resin applied-copper  
10 foil which is capable of manufacturing a printed wiring board  
without employing component materials of an insulating layer  
such as a prepreg, and to a copper-clad laminate and a printed  
wiring board which are excellent in flame retardancy.

15 BACKGROUND ART

A copper-clad laminate used for manufacturing a printed  
wiring board which is widely used in electric and electronic  
products is generally manufactured by employing the so-called  
prepreg, the prepreg being made by the impregnation of a glass  
20 cloth, kraft paper, a nonwoven glass fabric or the like with  
a thermosetting resin such as phenol resin or epoxy resin in  
order to make the resin in a semi-cured state, and by sticking  
and laminating the copper foil onto one side or both sides  
of the prepreg.

25 Further, in case of manufacturing a copper-clad laminate  
having three layers or more which is categorized as a  
multilayer printed wiring board, the copper-clad laminate is

manufactured by once performing the conductive circuit formation on a surface of the copper-clad laminate to make an internal layer base material, and by sticking the copper foil onto the both sides of the internal layer base material  
5 via the prepreg, for example.

In recent years, with the downsizing and greater packaging density of the printed wiring board, it has become common to provide fine blind holes, i.e., via holes, on a surface of the printed wiring board. As a method for forming  
10 this via holes, laser beam machining or plasma machining, for example, may be used. At this time, in a state that inorganic components like glass fibers are contained as frame materials in an insulating layer of the copper-clad laminate (for example, this state corresponds to a case of an insulating  
15 layer being comprised of a glass-epoxy prepreg which is referred to as an FR-4 base material.), the inorganic components as framework materials will affect the processability despite the ease of sublimation and evaporation of the resin component which are caused by the  
20 laser beam or plasma. Consequently, in order to allow uniform perforating, the insulating layer is frequently fabricated only with the resin components without employing the framework materials, to be used. Also, nonexistence of the frame materials results in a capability of eliminating  
25 influences of unevenness or ridges formed at a surface of the frame materials on a flatness of the copper-clad laminate, so that an extremely flat surface can be obtained. For

example, as for the above described FR-4 substrate, cloth grains of the glass cloth which is a framework material of the insulating layer develop on a surface of outer layer copper foil of the copper-clad laminate after being subjected  
5 to the hot press molding, so that in case of fabricating a thin resist layer such as a liquid resist, variations occur in a thickness of the resist layer, which consequently deteriorates a width precision of an etched circuit.

Therefore, these problems can be resolved by eliminating the  
10 framework materials.

In case of fabricating an insulating layer of a copper-clad laminate without including framework materials, manufacture of a multilayer copper-clad laminate is performed by any one of the following methods: (1) a method  
15 characterized in that a liquid resin is coated on a surface of an internal layer substrate and copper foil is stuck onto the resin, (2) a method characterized in that a resin film being comprised of a thermosetting resin in a semi-cured state is sandwiched between an inner layer substrate and copper foil  
20 to be stuck thereto, in order to perform thermoforming, (3) a method wherein resin applied-copper foil, i.e., copper foil having a resin layer formed thereon, is directly stuck to a surface of an inner layer substrate, or the like. Then the resultant product undergoes formation of the so-called outer  
25 layer circuits or formation of via holes, to be processed into a printed wiring board.

The above described method (1) has some problems, that is, it is difficult to more precisely and uniformly coat the liquid resin on a surface of the inner layer substrate on which inner layer circuits are already formed and uneven configurations are also formed, and in case of performing interlayer conducting plating when forming through holes or the like, it takes much time for grinding and removing the resin content which is deposited on an inner wall of the perforation or hole portion. And the resin film used in the above described method (2) is manufactured by coating a resin composition on a plastic film, however, costly plastic films to be discarded after its usage become enormous and thus a large amount of wastes are generated, so that from the view point of the environmental protection, this method is unacceptable in the present society wherein the environmental protection is taken very seriously.

Therefore, considering from the various view points, we have reached a conclusion that it is most advantageous to use resin applied-copper foil, and the above described method (3) is becoming widely and commonly pervasive. As a resin content used for the resin applied-copper foil, epoxy resins are frequently used. As for this resin applied-copper foil, the inventors have already proposed various resin applied-copper foil which are favorable for manufacturing the copper-clad laminate used for the printed wiring boards as a result of our intensive studies, and have widely contributed to the manufacture of high density printed wiring boards because

manufacturing the printed wiring boards with the use of this resin applied-copper foil allows easy forming of via holes or the like employing the laser processing method as well as forming of stable fine pitch circuits.

5       The copper-clad laminate manufactured by the use of such a resin applied-copper foil, when used for the printed wiring board, has practically satisfiable heat resistance, electric characteristics, and chemical resistant characteristics and has been widely supplied to the market.

10      As a resin used for the formation of resin layers of resin applied-copper foil which has conventionally been supplied to the market, epoxy halide resins or halogen based flame retarders are used in order to impart the flame retardancy. As for the demands for flame retardancy, it is required also 15 from a viewpoint of the PL Standards or the like to meet a certain criterion such that the ignition will not occur for the purpose of safety in electronic and electric equipment at the time of their usage.

20      As the criteria for this flame retardancy, there are various quality standards for the printed wiring boards, and each of home electrical products manufacturers and industrial electronics manufacturers etc. may often adopt its original criterion. Among others, a criterion defined in section 18 of the UL 796 which is also commonly referred to as "the UL 25 Standards", defining whether an item can be designated as a subject matter of insurance by the U.S. insurance company, has become a de facto standard as a practical global standard,

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and this criterion is one of the very important quality standards for the printed wiring boards. An evaluation test of the flame retardancy is conducted for a substrate from which noncombustible copper foil is removed after a 5 copper-clad laminate is manufactured. Therefore, a problem is not a flame retardancy required for the resin applied-copper foil itself, but a flame retardancy required for the copper-clad laminate from which the copper foil is removed, that is, the flame retardant characteristics of the resin 10 layer of the resin applied-copper foil which remains on the substrate side becomes a problem.

However, halogen elements added to the resin used for formation of the resin layers of the resin applied-copper foil has been reported to have an opportunity to generate toxic 15 compounds during the combustion treatment after being discarded, so that it has been required to develop resin compounds and resin applied-copper foil etc. which are free of halogen based flame retarders.

In order to try to solve this problem, as an alternative 20 to the halogen based flame retardar, it has been proposed to add inorganics such as phosphorous compounds represented by red phosphorous or phosphoric ester and metal hydroxides to the resin.

On the other hand, it has been pointed out that water 25 resistance and heat resistance of the resin become worse when the phosphorous compounds are used, so that there is a possibility that the safety reliability of the printed wiring

boards at the time of their manufacturing process and their usage is deteriorated. Further, the resin composition becomes hard and brittle when the metal hydroxide is used and the peel strength between the resin and the copper foil is 5 substantially reduced, consequently there has been a problem that faulty adherence occurs between the base material and the copper foil.

Therefore, it has been required to be able to form a resin layer of resin applied-copper foil employing a resin compound 10 which is free of halogen elements and to manufacture a copper-clad laminate without any of above described problems, and to provide high flame retardancy, excellent water resistance and heat resistance, and good peel strength between a base material and copper foil.

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#### DISCLOSURE OF THE INVENTION

Hence, the inventors have developed a resin compound which will be described hereinafter and also developed a resin sheet and resin applied-copper foil which use this resin 20 compound as a result of our intensive studies. Further, manufacturing a copper-clad laminate by the use of above described materials allows a printed wiring board to be provided which is excellent in both characteristics, that is, heat resistance and flame resistance.

25 Firstly, the present invention as set forth in claim 1 is a resin compound for fabricating an interlayer dielectric of a printed wiring board, wherein the resin compound has a

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composition comprising an epoxy based resin which includes an epoxy resin curing agent having 5 to 25% by weight of nitrogen and maleimide compounds which have thermosetting properties (possible to limit the content?) and being free of 5 halogen elements, and that the resin compound is formed by dissolving the composition in an organic solvent.

According to the present invention, when the nitrogen content in the curing agent within components of the epoxy based resin which constitutes the resin compound for 10 fabricating the interlayer dielectric is 5 to 25 % by weight, good performance can be delivered in terms of the flame retardancy and the water absorption, so that the selective usage of proper curing agent for the epoxy based resin allows the cured epoxy resin to have a self-digesting characteristic.

15 In addition, the present invention is to provide a resin compound for fabricating an interlayer dielectric having higher heat resistance and flame retardancy, in combination with the use of maleimide compounds having higher flame retardancy by itself with a thermosetting property. Further,

20 this composition makes it possible to eliminate halogen elements represented by chlorine etc. which are added to the compound in order to impart the flame retardancy, so that it becomes possible to reduce loads to the natural environment in a stage of discarding the copper-clad laminate and the 25 printed wiring board.

The resin compound for fabricating the interlayer dielectric as set forth in claim 1 is described as one

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basically comprised of the epoxy based resin and the maleimide compounds. The epoxy based resin as described herein means a resin which uses epoxy resins as a base material and contains at least a resin curing agent required for curing the epoxy 5 resin, and is also assumed to include other resin components such as melamine resin or phenol resin, an accelerator, an antifoaming agent, and a leveling agent, etc. which are added as necessary. These additional components can control the curing rate of the resin and produce an effect of the cost 10 reduction. This is because, as a general concept in the chemical context, it becomes impossible to readily conduct the curing of the epoxy resin if the epoxy resin curing agent is not included. The maleimide compounds mentioned in the present invention will be described in detail in a description 15 of the resin compound for fabricating the interlayer dielectric as set forth in claim 2.

In claim 1, a sentence "comprising an epoxy based resin which includes an curing agent having 5 to 25% by weight of nitrogen and maleimide compounds which have thermosetting properties" is described. This sentence is described as a concept including not only a resin compound for fabricating an interlayer dielectric obtained by mixing "an epoxy based resin which includes a curing agent having 5 to 25 % by weight of nitrogen" with "maleimide compounds which have 20 thermosetting properties" each of which is separately produced but also a resin compound for fabricating an 25 interlayer dielectric obtained by simultaneously adding the

maleimide compounds when the epoxy resin and the above described epoxy resin curing agent, etc. are dissolved. That is, there is no particular restrictions on the order of mixing the constituent compounds when producing the resin compound used for fabricating the interlayer dielectric.

A solvent used for the dissolution will be described in the following description of a method for manufacturing. The above described resin compound for fabricating the interlayer dielectric is used for forming an insulating resin layer between the copper foil circuit layers of the copper-clad laminate.

In addition, as defined in claim 2 that the resin used  
for fabricating the interlayer dielectric of the printed  
wiring board as set forth in claim1, wherein the epoxy based  
resin comprises epoxy resins having two or more glycidyl  
groups per molecule, polymers having crosslinkable  
functional groups within a molecule, a crosslinker which is  
added as necessary, and a phenol novolak epoxy resin curing  
agent containing triazine rings within a molecule, it is  
desirable to use the resins described above as epoxy resins  
used in the present invention.

An epoxy resin having two or more glycidyl groups per molecule is used as the epoxy resin. If an epoxy resin having one glycidyl group per molecule is used, a crosslinking state of the resin tends to be insufficient and results in lowering of the flame retardancy, so that an object of the present invention cannot be achieved. Although an epoxy resin which

is generally used for electric and electronic materials can be used without any particular restrictions as far as the above described condition is satisfied, an epoxy resin which is substantially free of halogens is preferable to be used  
5 in this context.

An epoxy resin having two or more glycidyl groups per molecule is desirably 20 to 70 parts by weight given that the total amount of the resin compound is 100 parts by weight. If the blending proportion of the epoxy resin is less than  
10 20 parts by weight, the adhesive property between the copper foil and the base material after being processed to the copper-clad laminate becomes lower and the peel strength also tends to be decreased. By contrast, if the blending proportion of the epoxy resin is 70 parts by weight or more,  
15 flowability of the resin compound becomes too much to treat the compound, so that it becomes difficult to control a layer thickness when a resin layer is formed on the copper foil or a resin sheet described below is manufactured.

Therefore, as defined in claim 3 that the resin used for  
20 fabricating the interlayer dielectric of the printed wiring board as set forth in claim 2, wherein the epoxy resins having two or more glycidyl groups per molecule are free of halogen elements and are any one or more of bisphenol A epoxy resin, bisphenol F epoxy resin, novolak epoxy resin, cresol novolak  
25 epoxy resin, and glycidylamine epoxy resin, the epoxy resins described herein which are free of halogen elements are most preferable to be used. These are capable of exploiting the

most stable substrate performance from a broad view in an application for manufacturing the printed wiring board, in terms of not only the flame resistance but also various characteristics including the peel strength between the base material and the copper foil and the chemical resistance.

"Polymers having crosslinkable functional groups within a molecule" in a sentence "polymers having crosslinkable functional groups within a molecule and a crosslinker which is added as necessary" as set forth in claim 2 is used for preventing cracks from occurring in a resin layer when the resin compound is coated on the copper foil to form the resin layer on the copper foil and processed to a resin applied-copper foil, preventing resin powder from scattering at the time of cutting and crushing after being processed to the copper-clad laminate, and ensuring a certain range of flowability by performing the viscosity control of the resin compound before forming the resin layer.

As for the polymers, as defined in claim 4, it is preferable to use any one or more of polyether sulfone resin having a hydroxyl group at a terminal, polyvinyl acetal resin having repeated hydroxyl groups within a molecule, and phenoxy resin, as the polymers which have crosslinkable functional groups within a molecule.

There is not necessary to particularly limit the polymer as described above as far as the polymer corresponds to the above described polyether sulfone resin having a hydroxyl group at a terminal, polyvinyl acetal resin having repeated

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hydroxyl groups within a molecule, or phenoxy resin. If a sufficient crosslinking reaction can be allowed to proceed by the use of polymer with crosslinkable functional groups within a molecule such as the hydroxyl groups in the polymers  
5 described above, highly excellent heat resistance can be imparted to the copper-clad laminate or the printed wiring board being manufactured by using thereof, even when the resin compound is cured and becomes a part of the copper-clad laminate. Therefore, in case of using a resin compound which  
10 uses a polymer having no crosslinkable functional groups within a molecule, the heat resistance after curing the resin compound becomes significantly lower, so that the compound may not be used.

In addition, the polymer having crosslinkable  
15 functional groups within a molecule is desirable to be in a range of 5 to 30 parts by weight given that the total amount of the resin compound is 100 parts by weight. The effects of preventing cracks from occurring and preventing the resin powder from scattering cannot be produced when the polymer  
20 is less than 5 parts by weight, whereas the flowability of the resin becomes too low when the polymer is 30 parts by weight or more, so that controlling the layer thickness becomes difficult when the resin layer is formed on the copper foil or when a resin sheet described below is manufactured, as in  
25 the case where the amount of epoxy resin becomes excessive.

"A crosslinker which is added as necessary" is used depending on a kind of polymer, that is, blocked isocyanate

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is used for bisphenol A epoxy resin for example and other crosslinkers should be considered to be used as appropriate, so that there is not necessary to impose particular limitations on the above described crosslinkers. In  
5 addition, the present invention does not always use the crosslinker. Because, in case of using polyether sulfone resin as a polymer for example, a crosslinking reaction with the epoxy resin can be conducted without adding the crosslinker separately.

10 "As a phenol novolak epoxy resin curing agent containing triazine rings within a molecule" as set forth in claim 2, one comprised of one or two of melamine and benzoguanamine and a compound obtained from a condensation reaction of phenols and formaldehyde, and having 5 to 25% by weight of  
15 nitrogen content is most preferably employed as defined in claim 5. More specifically, the curing agent is, for example, an AT novolak resin having a trade name of LA-7054 manufactured by Dainippon Ink Inc. The resin compound according to the present invention, which uses the above  
20 described compounds as a curing agent of the epoxy resin, provides a self-digesting characteristic.

The usage amount of the phenol novolak epoxy resin curing agent which contains triazine rings within a molecule should not be specified to a certain amount which is particularly  
25 limited because this amount is calculated from an equivalent ratio to the epoxy resin to be used and from experimental data.

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As maleimide compounds, it is most preferable to use maleimide compounds having thermosetting properties as set forth in claim 6. That is, the compounds are, for example, N,N'-(diphenylmethane)bismaleimide, bis(3-ethyl-5-methyl-5-maleimide)methane, and 2,2-bis[4-(4-maleimidophenoxy)phenyl]propane. Still further, it is possible to obtain good results by the use of a thermosetting maleimide compound which can be obtained by Michael addition reaction of the above described maleimide compound with polyamides.

A content of the maleimide compound having a thermosetting property in the resin compound according to the present invention is desirable to be 10 to 50 parts by weight given that a total amount of the resin compound is 100 parts by weight. If the maleimide compound is less than 10 parts by weight, an intended sufficient flame retardancy cannot be obtained when the resin compound according to the present invention is cured as an insulating layer of the copper-clad laminate. By contrast, if 50 parts by weight or more of the maleimide compound is used, the cured resin becomes extremely brittle and its mechanical characteristics also become worse, so that the reliability for shock resistance or load capacity etc. of the resultant printed wiring board is compromised. Such a worsening in the mechanical characteristics becomes an extremely critical defect for a printed wiring board to which a load of a flyback transformer having several kilograms

of loads is directly applied, such as a mother board being built in a television for example.

The resin compound according to the present invention as described above, which is used as a material for 5 fabricating the interlayer dielectric of the copper-clad laminate, makes it possible to impart excellent heat resistance and flame resistance to a printed wiring board which is obtained from the copper-clad laminate.

As defined in claim 7, a method for producing the resin 10 compound used for fabricating the interlayer dielectric of the printed wiring board as set forth in any of claims 1 to 6, wherein a composition is made to have 20 to 70 parts by weight of epoxy resins, 5 to 30 parts by weight of polymers having crosslinkable functional groups within a molecule, 10 15 to 50 parts by weight of maleimide compounds having thermosetting properties, and a balance of a crosslinker added as necessary and a phenol novolak epoxy resin curing agent containing triazine rings within a molecule given that a total amount of the resin compound excluding a solvent is 20 100 parts by weight, and that a solids content after the composition is added to and dissolved in the solvent becomes 30 to 80% by weight, can be derived from the blending proportion used for obtaining the resin compound according to the present invention.

25 The meanings of blending proportion of respective resin components and a curing agent etc. are as described above. And a reason for defining as "a solids content after the

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composition is added to and dissolved in the solvent becomes 30 to 80% by weight" in this claim 7 is that a proper viscosity range which is capable of favorably controlling the resin layer thickness can be obtained within this range when a resin  
5 applied-copper foil is formed or a resin sheet is formed. That is, if the solids are less than 30% by weight, the viscosity of the resin becomes lower and its flowability becomes too large, so that a coating thickness of the resultant resin layer is excessively reduced. By contrast,  
10 if the solids exceed 80% by weight, the viscosity of the resin becomes higher and its flowability becomes too low, so that a coating thickness of the resultant resin layer is excessively increased.

In addition, as a solvent used for obtaining the resin  
15 compound according to the present invention, as defined in claim 8, it is preferable to use a mixed solvent of N-methylpyrrolidone and methyl ethyl ketone which has a mixing ratio of N-methylpyrrolidone/methyl ethyl ketone=50/50 to 40/60 (by weight).

20 That is, as a solvent generally used for dissolving a resin according to the present invention, it is desirable to use a single component such as methyl ethyl ketone which is readily volatilized during a drying process. However, constituents of the resin according to the present invention  
25 include maleimide compounds, so that it is almost impossible to dissolve the compounds with the use of methyl ethyl ketone only. Therefore, the inventors have contemplated the use of

the mixed solvent of N-methylpyrrolidone and methyl ethyl ketone.

According to a comparison of a property of this methyl ethyl ketone with that of N-methylpyrrolidone, a boiling point of the methyl ethyl ketone is 79.6°C, whereas a boiling point of the N-methylpyrrolidone is around 200°C. Thus, it can be said that the N-methylpyrrolidone is more resistant to be volatilized than the methyl ethyl ketone. For these reasons, a usage amount of N-methylpyrrolidone should be within a certain range in which the maleimide compounds used for the present invention can be dissolved and should be minimized.

As mentioned above, the inventors have decided as a result of our intensive studies that the maleimide compounds used for the present invention can be readily dissolved in the mixed solvent which includes a certain amount of N-methylpyrrolidone, that is, a ratio of N-methylpyrrolidone/methyl ethyl ketone in the mixed solvent is at least 40/60 (by weight). If the ratio of N-methylpyrrolidone/methyl ethyl ketone exceeds 50/50 (by weight), a volatilization speed which is usually required is not satisfied, so that the industrial productivity is not satisfied.

The following method is contemplated when the interlayer dielectric of the copper-clad laminate is fabricated by the use of these resin compounds. A resin sheet which is processed in a semi-cured state is inserted between an inner

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layer base material and outer layer copper foil as in the case of employing a prepreg, then subjected to the hot press molding in order to be able to obtain a copper-clad laminate. Therefore, claim 9 defines that the resin compound for 5 fabricating the interlayer dielectric of the printed wiring board as set forth in any of claims 1 to 6 is a resin sheet in a semi-cured state for forming an insulating layer for manufacturing the copper-clad laminate. Further, claim 11 defines that the copper-clad laminate is manufactured by the 10 use of the resin sheet for forming the insulating layer as set forth in claim 9.

The method for processing the resin compound into the resin sheet may be a method for processing the resin compound according to the present invention being in a semi-cured state 15 into a sheet or a method wherein a resin layer having a predetermined thickness is formed on a plastic film as a carrier, and the carrier is peeled off at the time of usage.

Further, claim 10 defines that the resin applied-copper foil with the resin layer formed on a surface of the copper 20 foil by the use of the resin for fabricating the interlayer dielectric of the printed wiring board as set forth in any of claims 1 to 6, and claim 12 defines that the copper-clad laminate is manufactured by the use of the resin applied-copper foil as set forth in claim 10.

25 The above mentioned matters are claimed because the resin compound according to the present invention can be used for manufacturing the resin applied-copper foil and this resin

applied-copper foil can be used for manufacturing the copper-clad laminate.

As for the manufacture of the resin applied-copper foil, a semi-cured resin layer is formed on a surface of the copper  
5 foil by coating the resin compound according to the present invention on an adhesive surface of the copper foil to the inner layer base material, with the use of the resin coating apparatus referred to as so-called an edge coater or a roll coater, to a predetermined thickness, then drying the resin  
10 compound.

Using this resin applied-copper foil like the common copper foil, it becomes possible to manufacture the copper-clad laminate without the use of materials for fabricating the insulating layer such as a prepreg.

15 Thus obtained copper-clad laminate, since framework materials are not included as in the case of the FR-4 prepreg, is excellent in surface smoothness, possible to provide good registration, easy to form fine pitch circuits, and excellent in formation accuracy of via holes through the laser machining,  
20 and also excellent in heat resistance and flame resistance.

#### BEST MODE FOR CARRYING OUT THE INVENTION

The present invention is described below in more detail, while describing the examples according to the present  
25 invention.

Example 1: In this example, a resin compound was obtained through blending 30 parts by weight of a polymer blend, 30

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parts by weight of an epoxy resin having two or more glycidyl groups per molecule, 21 parts by weight of a maleimide compound having a thermosetting property, and 19 parts by weight of a phenol novolak epoxy resin curing agent containing 5 triazine rings within a molecule. Each of the blending proportions stated herein shows a proportion based on a solids content.

The polymer blend herein means a mixture of a polymer having crosslinkable functional groups within a molecule and 10 its crosslinker. Specifically, the polymer blend was formed by mixing bisphenol A phenoxy resin, which has hydroxyl groups as functional groups and has a weight average molecular weight of 4800 based on polystyrene included, with blocked isocyanate as the crosslinker (Collonate AP, made by Nihon 15 Polyurethane Inc., trade name), in a ratio of 10:2 (by weight).

As the epoxy resin having two or more glycidyl groups per molecule, O-cresol epoxy resin having an epoxy equivalent of 195 was used.

20 As the maleimide compound having a thermosetting property, N,N'-(4,4-diphenylmethane)bismaleimide was used.

As the phenol novolak epoxy resin curing agent containing triazine rings within a molecule, LA-7054 (made by Dainippon Ink and Chemicals, Inc. AT novolak resin) was used.

25 Then, the thus blended above described resin was added to a mixed solvent having a ratio of N-methylpyrrolidone/methyl ethyl ketone=50/50 (by weight),

stirred and dissolved so that the solids became 40% by weight, then the resin compound was obtained.

Example 2: In manufacture of a resin compound in this example, blending proportions which were basically similar 5 to those used in Example 1 were used. Therefore, only different parts will be described and the same descriptions as in the case of Example 1 will be omitted.

The different part is that polyether sulfone resin having a hydroxyl group at a terminal of the molecule was used instead 10 of the polymer blend used in Example 1. In this case, a crosslinker was not particularly added to the polyether sulfone resin separately because this polyether sulfone resin caused a crosslinking reaction with the epoxy resin without the addition of any crosslinker. This blend was processed 15 into a resin applied-copper foil, then a multilayer copper-clad printed wiring board was obtained according to the method similar to Example 1.

Example 3: In this example, a resin compound was produced by making a modification to the blending proportion of a resin 20 used in Example 1, so that in this example, only the blending proportion was different from above-described examples. Therefore, only the blending proportion will be described and the same descriptions as in the previous Examples will be omitted.

25 The blending proportions were 20 parts by weight of a polymer blend, 40 parts by weight of O-cresol epoxy resin, 26 parts by weight of N,N'-(4,4-

diphenylmethane)bismaleimide, and 14 parts by weight of AT novolak resin. The proportions were obtained based on a solids content, which is also the same as in the case of Example 1.

5       The inventors further manufactured a resin compound which was used for comparing the performance of a resin compound according to the present invention with that of the conventional level. These compounds are described in the following Comparative Examples 1 to 3.

10      Comparative Example 1: A resin compound was obtained by employing the same kind of resin as used in Example 1 and by making a modification to the blending proportion of each resin as follows.

15      The blending proportions in this case were 30 parts by weight of a polymer blend, 43 parts by weight of O-cresol epoxy resin, and 27 parts by weight of AT novolak resin. These values were also obtained based on a solids contet.

20      Comparative Example 2: A resin compound was obtained by the use of polyether sulfone having no reactive functional groups instead of the polymer blend used for Example 1. The blending proportions and the manufacturing conditions in this case were the same as those of Example 1.

25      Comparative Example 3: A resin compound was obtained by the use of a commercially available cresol novolak epoxy resin curing agent instead of AT novolak resin used for Example 1. The blending proportions and the manufacturing conditions in this case were the same as those of Example 1.

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In order to verify the performance of the resin compounds obtained in the above-described Examples 1 to 3 and Comparative Examples 1 to 3, each of these resin compounds was coated on a matte side of electrolytic copper foil having 5 a nominal thickness of 18  $\mu\text{m}$ , then air-dried, and heated at 160°C for 5 minutes to obtain a resin applied-copper foil having a semi-cured resin layer. The thickness of the resin layer at this time was 80 to 82  $\mu\text{m}$ . This resin applied-copper foil was laminated to both sides of the FR-4 inner layer base 10 material (a core thickness 0.5 mm, copper foil thickness 35  $\mu\text{m}$ ) on which a predetermined circuit was formed, through the hot press molding. The resin applied-copper foil was overlaid such that its resin layer was in contact with the inner layer base material, and subjected to the hot press 15 molding for two hours with applying a pressure of 20 kgf/cm<sup>2</sup> and under the temperature of 180°C, then a multilayer copper-clad laminate having four copper foil layers was obtained.

Then this multilayer copper-clad laminate was used to 20 carry out the flammability test based on the UL796 Standards and the UL94 in order to compare their flame resistance. Procedures of this test carried out was as follows. A sample for the flammability test took a size of 127 mm in length and 12.7 mm in width, and was processed to be in a smooth shape 25 at its edge portion. At this time, the copper foil which was a conductive material having a nominal thickness of 18  $\mu\text{m}$  and was disposed as an outer layer was etched off, so that the

sheet thickness after removing the outer layer copper foil was 150  $\mu\text{m}$ .

In order to evaluate the heat resistance, a soldering bus at a temperature of 260°C was used to carry out the 5 soldering heat test based on section 5.5 of the JIS C 6481 without the outer layer copper foil being removed, and a time that the copper-clad laminate was blistered was measured.

The result is shown in Table 1. As can be seen from this table, when Comparative Examples 1 to 3 are compared with 10 Examples 1 to 3, there are no samples which have both of the soldering heat resistance and the flame resistance in case of Comparative Examples, whereas samples in case of Examples have both characteristics of the soldering heat resistance and the flame resistance, so that it becomes possible to 15 manufacture a copper-clad laminate being excellent in its total balance.

Table 1

Sample	Soldering Heat Resistance	Flame Resistance (UL Flammability Test)
	Second	Grade
First Embodiment	120 or more	94V-0
Second Embodiment	120 or more	94V-0
Third Embodiment	120 or more	94V-0
Comparative Example 1	120 or more	94V-1
Comparative Example 2	20	94V-0
Comparative Example 3	120 or more	94V-1

20 The 94V-0 grade which represents the flame resistance is defined as follows. That is, the copper-clad laminate

sample is firstly contacted to a flame of a burner for 9.5 to 10.5 seconds under the conditions defined in the standard, then an after-flaming time ( $t_1$ ) which is the time required until the flame is extinguished after the burner is separated from the sample by a predetermined distance, an after-flaming time ( $t_2$ ) after the sample is secondary contacted to the flame of the burner in the same manner as described above, and a smoke-remaining time ( $t_3$ ) are measured. In this case, the 94V-0 grade means that each of five samples making a set satisfies the following conditions: both of  $t_1$  and  $t_2$  are 10 seconds or less,  $t_1 + t_2$  is 50 seconds or less,  $t_2 + t_3$  is 30 seconds or less; flame or smoke which remains at a clamp holding the sample cannot be observed, and inflammable substance or dropping cannot be found in a predetermined cotton which is used as a pilot.

By contrast, 94V-1 grade is defined as follows. That is, the copper-clad laminate sample is firstly contacted to a flame of a burner for 9.5 to 10.5 seconds under the conditions defined in the standard, then an after-flaming time ( $t_1$ ) which is the time required until the flame is extinguished after the burner is separated from the sample by a predetermined distance, an after-flaming time ( $t_2$ ) after the sample is secondary contacted to the flame of the burner in a similar manner as above, and a smoke-remaining time ( $t_3$ ) are measured. In this case, the 94V-1 grade means that each of five samples making a set satisfies the following conditions: both of  $t_1$  and  $t_2$  are 30 seconds or less,  $t_1 + t_2$  is 250 seconds or less,

$t_2 + t_3$  is 60 seconds or less; flame or smoke which remains at a clamp holding the sample cannot be observed, and inflammable substance or dropping cannot be found in a predetermined cotton which is used as a pilot. Therefore,  
5 the flame resistance for the 94V-0 grade is more critical than that for the 94V-1, so that the copper-clad laminate using the resin compound according to the present invention is found to be excellent in its heat resistance and to have high flame retardancy.

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#### INDUSTRIAL APPLICABILITY

Fabricating an interlayer dielectric of a copper-clad laminate by the use of a resin compound according to the present invention largely improves both of the heat  
15 resistance and the flame resistance regarding to the copper-clad laminate or a printed wiring board, makes it possible to form a fine-pitch circuit and to provide a copper-clad laminate on which laser perforating is easily conducted, and further allows the safety reliability during  
20 a manufacturing process and at the usage of the printed wiring board to be extremely high. Therefore, inflammable accidents happened to home electrical products and to various kinds of electronic products can be prevented, and products can be supplied in excellent condition also from a viewpoint  
25 of the product liability. Still further, the resin compound according to the present invention is free of halogen elements,

so that the compound is desirable also from a viewpoint of  
the natural environmental protection.